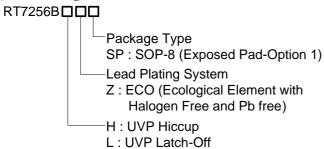


# 3A, 17V, 1.2MHz Synchronous Step-Down Converter

### **General Description**

The RT7256B is a high efficiency, monolithic synchronous step-down DC/DC converter that can deliver up to 3A output current from a 4.5V to 17V input supply. The RT7256B's current mode architecture and internal compensation allow the transient response to be optimized over a wide input range and loads. Cycle-by-cycle current limit provides protection against shorted outputs, and soft-start eliminates input current surge during start-up. The RT7256B also provides under voltage protection and thermal shutdown protection. The low current (<3µA) shutdown mode provides output disconnection, enabling easy power management in battery-powered systems. The RT7256B is available in an SOP-8 (Exposed Pad) package.

## **Ordering Information**



#### Note:

Richtek products are:

- ▶ RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- ▶ Suitable for use in SnPb or Pb-free soldering processes.

## **Marking Information**



RT7256BxZSP: Product Number

x: H or L

YMDNN: Date Code

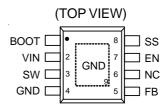
#### **Features**

- ±1.5% High Accuracy Reference Voltage
- 4.5V to 17V Input Voltage Range
- **3A Output Current**
- Integrated N-MOSFET Switches
- Current Mode Control
- Fixed Frequency Operation: 1.2MHz
- Output Adjustable from 0.8V to 12V
- Up to 95% Efficiency
- Programmable Soft-Start
- Stable with Low ESR Ceramic Output Capacitors
- Cycle-by-Cycle Over Current Protection
- Input Under Voltage Lockout
- Output Under Voltage Protection
- Thermal Shutdown Protection
- **RoHS Compliant and Halogen Free**

### **Applications**

- Wireless AP/Router
- Set-Top-Box
- Industrial and Commercial Low Power Systems
- LCD Monitors and TVs
- Green Electronics/Appliances
- Point of Load Regulation of High-Performance DSPs

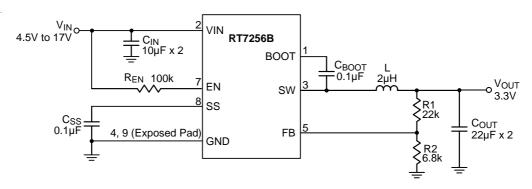
## **Pin Configurations**



SOP-8 (Exposed Pad)



# **Typical Application Circuit**



**Table 1. Suggested Component Selection** 

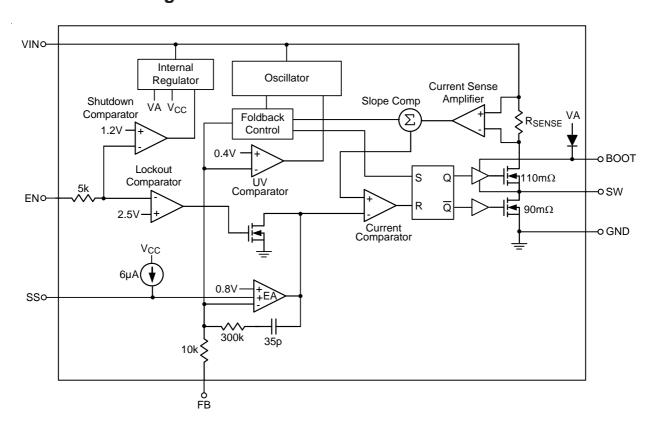
V <sub>OUT</sub> (V)	R1 (kΩ)	R2 (kΩ)	L (μH)	C <sub>OUT</sub> (μF)	
8	9	1	3.6	22 x 2	
5	10.5	2	2	22 x 2	
3.3	22	6.8	2	22 x 2	
2.5	25.5	12	1	22 x 2	
1.8	31.25	25	0.68	22 x 2	
1.2	35.7	68	0.68	22 x 2	

**Functional Pin Description** 

Pin No.	Pin Name	Pin Function
1	воот	Bootstrap for High Side Gate Driver. Connect a $0.1\mu F$ or greater ceramic capacitor from BOOT to SW pins.
2	VIN	Input Supply Voltage, 4.5V to 17V. Must bypass with a suitably large ceramic capacitor.
3	SW	Switch Node. Connect this pin to an external L-C filter.
4, 9 (Exposed Pad)	GND	Ground. The exposed pad must be soldered to a large PCB and connected to GND for maximum power dissipation.
5	FB	Feedback Input. It is used to regulate the output of the converter to a set value via an external resistive voltage divider.
6	NC	No Internal Connection.
7	EN	Enable Input Pin. A logic high enables the converter; a logic low forces the RT7256B into shutdown mode reducing the supply current to less than $3\mu$ A. Attach this pin to VIN with a $100k\Omega$ pull up resistor for automatic startup.
8	Soft-Start Control Input. SS controls the soft-start period. Connect a cap from SS to GND to set the soft-start period. A 0.1μF capacitor set soft-start period to 13.5ms.	



# **Function Block Diagram**





## Absolute Maximum Ratings (Note 1)

• Supply Voltage, V <sub>IN</sub>	-0.3V to 20V
Switch Voltage, SW	$-0.3V$ to $(V_{IN} + 0.3V)$
• V <sub>BOOT</sub> – V <sub>SW</sub>	-0.3V to 6V
Other Pins Voltages	-0.3V to 20V
<ul> <li>Power Dissipation, P<sub>D</sub> @ T<sub>A</sub> = 25°C</li> </ul>	
SOP-8 (Exposed Pad)	1.333W
Package Thermal Resistance (Note 2)	
SOP-8 (Exposed Pad), $\theta_{JA}$	75°C/W
SOP-8 (Exposed Pad), $\theta_{JC}$	15°C/W
• Lead Temperature (Soldering, 10 sec.)	260°C
Junction Temperature	150°C
Storage Temperature Range	-65°C to 150°C
ESD Susceptibility (Note 3)	
HBM (Human Body Mode)	2kV
MM (Machine Mode)	200V
Recommended Operating Conditions (Note 4)	
• Supply Voltage, V <sub>IN</sub>	4.5V to 17V

• Ambient Temperature Range ----- --- -40°C to 85°C

#### **Electrical Characteristics**

( $V_{IN} = 12V$ ,  $T_A = 25$ °C, unless otherwise specified)

Parameter	Symbol	Test Conditions	Min	Тур	Max	Unit
Shutdown Supply Current		V <sub>EN</sub> = 0V		0.5	3	μΑ
Supply Current		V <sub>EN</sub> = 3V, V <sub>FB</sub> = 0.9V		0.8	1.2	mA
Reference Voltage	V <sub>REF</sub>	$4.5V \le V_{IN} \le 17V$	0.788	0.8	0.812	V
High Side Switch On-Resistance	R <sub>DS(ON)1</sub>			110		mΩ
Low Side Switch On-Resistance	R <sub>DS(ON)2</sub>			90		mΩ
High Side Switch Leakage Current		$V_{EN} = 0V, V_{SW} = 0V$		0	10	μΑ
Upper Switch Current Limit		Min. Duty Cycle, VBOOT – VSW = 4.8V		5.1		Α
COMP to Current Sense Transconductance	G <sub>CS</sub>			4.7		A/V
Oscillation Frequency	fosc1		1000	1200	1400	kHz
Short Circuit Oscillation Frequency	f <sub>OSC2</sub>	V <sub>FB</sub> = 0V		270		kHz
Maximum Duty Cycle	D <sub>MAX</sub>	V <sub>FB</sub> = 0.7V		78		%
Minimum On-Time	ton			100		ns

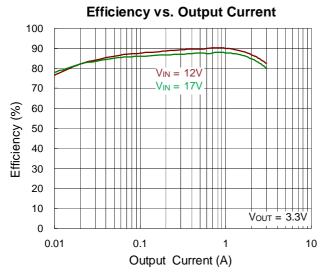


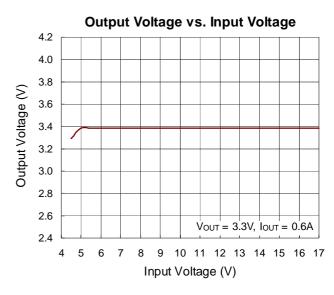
Parameter		Symbol	Test Conditions	Min	Тур	Max	Unit
EN Input	Logic-High	VIH		2.7		17	3.7
Threshold Voltage	Logic-Low	V <sub>IL</sub>				0.4	V
Input Under Volta Threshold	Input Under Voltage Lockout Threshold		V <sub>IN</sub> Rising	3.8	4.2	4.5	V
Input Under Voltage Lockout Hysteresis		$\Delta V_{UVLO}$			320		mV
Soft-Start Current		I <sub>SS</sub>	$V_{SS} = 0V$		6		μΑ
Soft-Start Period		tss	C <sub>SS</sub> = 0.1μF		13.5		ms
Thermal Shutdown		T <sub>SD</sub>			150		°C

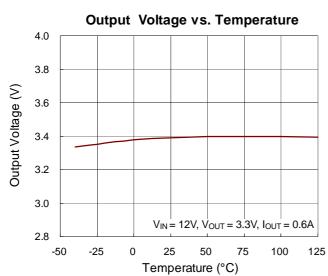
- **Note 1.** Stresses beyond those listed "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.
- Note 2.  $\theta_{JA}$  is measured at  $T_A = 25^{\circ}C$  on a high effective thermal conductivity four-layer test board per JEDEC 51-7.  $\theta_{JC}$  is measured at the exposed pad of the package.
- Note 3. Devices are ESD sensitive. Handling precaution is recommended.
- Note 4. The device is not guaranteed to function outside its operating conditions.

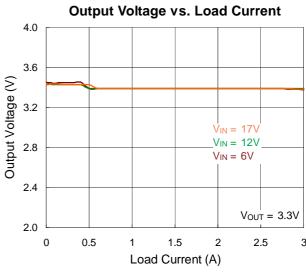


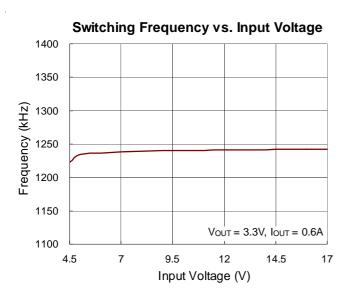
## **Typical Operating Characteristics**

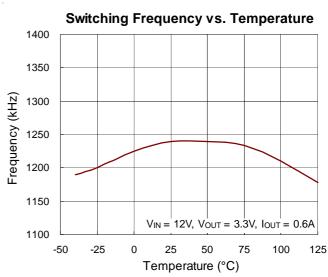






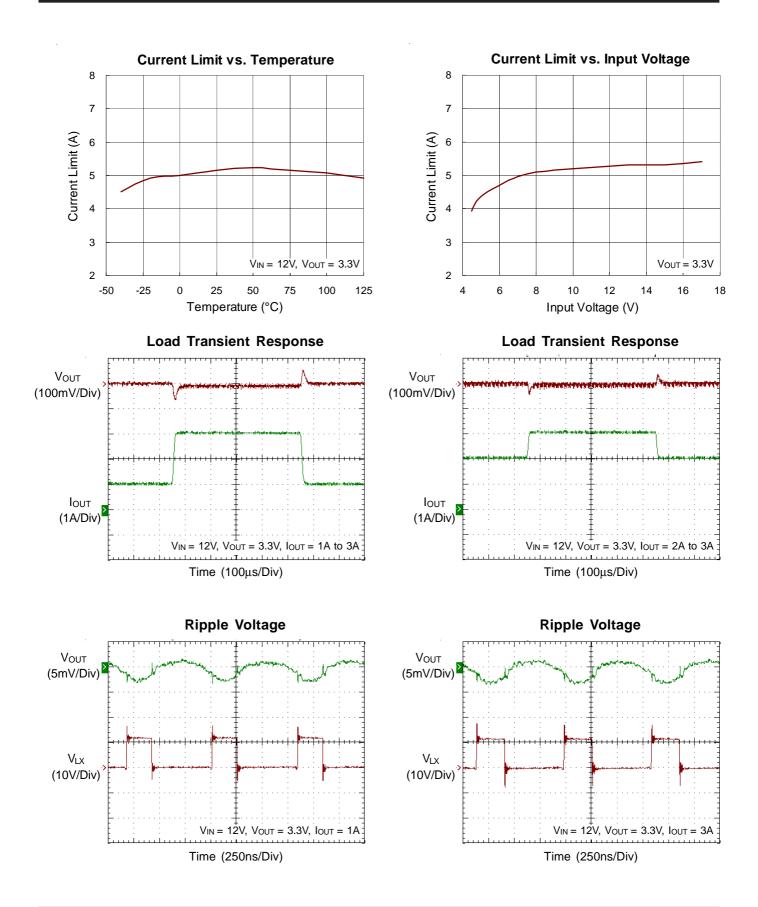






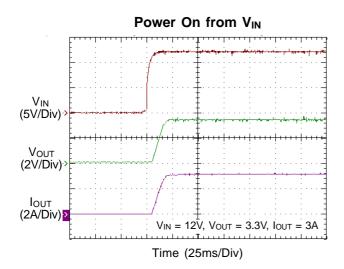
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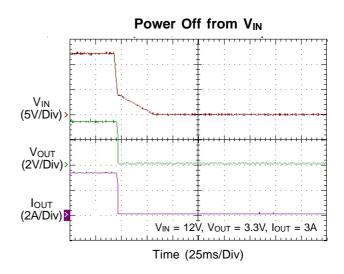


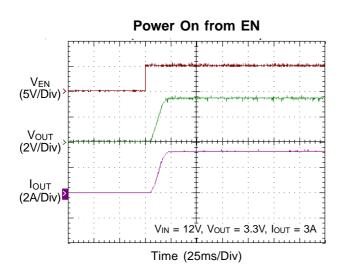


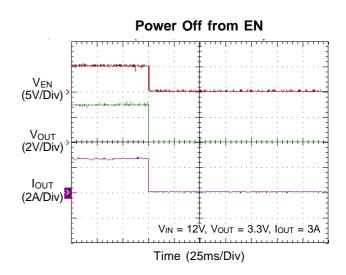
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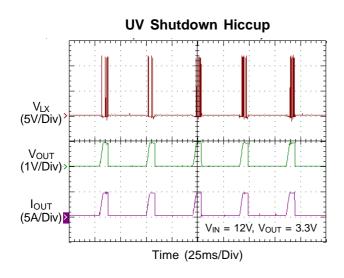


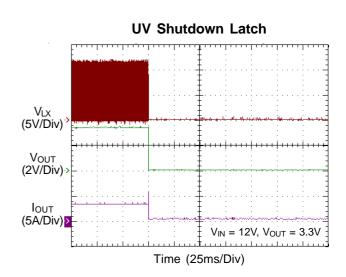














### **Application Information**

#### **Output Voltage Setting**

The resistive divider allows the FB pin to sense the output voltage as shown in Figure 1.

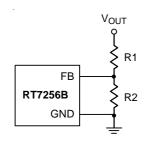


Figure 1. Output Voltage Setting

The output voltage is set by an external resistive voltage divider according to the following equation:

$$V_{OUT} = V_{REF} \left( 1 + \frac{R1}{R2} \right)$$

Where  $V_{REF}$  is the reference voltage (0.8V typ.).

#### **External Bootstrap Diode**

Connect a  $0.1\mu F$  low ESR ceramic capacitor between the BOOT pin and SW pin. This capacitor provides the gate driver voltage for the high side MOSFET.

It is recommended to add an external bootstrap diode between an external 5V and BOOT pin for efficiency improvement when input voltage is lower than 5.5V or duty ratio is higher than 65% .The bootstrap diode can be a low cost one such as IN4148 or BAT54. The external 5V can be a 5V fixed input from system or a 5V output of the RT7256B. Note that the external boot voltage must be lower than 5.5V

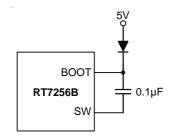


Figure 2. External Bootstrap Diode

#### Soft-Start

The RT7256B provides soft-start function. The soft-start function is used to prevent large inrush current while converter is being powered-up. The soft-start timing can be programmed by the external capacitor between SS and GND. An internal current source  $I_{SS}$  (6 $\mu A$ ) charges an external capacitor to build a soft-start ramp voltage. The  $V_{FB}$  voltage will track the internal ramp voltage during soft-start interval. The typical soft-start time is calculated as follows :

Soft-Start time 
$$t_{SS} = \frac{0.8 \times C_{SS}}{I_{SS}}$$
, if  $C_{SS}$  capacitor is  $0.1 \mu F$ , then soft-start time =  $\frac{0.8 \times 0.1 \mu}{6 \mu} = 13.5 ms$ 

#### **Chip Enable Operation**

The EN pin is the chip enable input. Pulling the EN pin low (<0.4V) will shut down the device. During shutdown mode, the RT7256B quiescent current drops to lower than 3 $\mu$ A. Driving the EN pin high (>2.7V, 17V) will turn on the device again. For external timing control, the EN pin can also be externally pulled high by adding a R<sub>EN</sub> resistor and C<sub>EN</sub> capacitor from the VIN pin (see Figure 3).

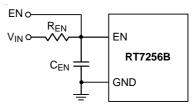


Figure 3. Enable Timing Control

An external MOSFET can be added to implement digital control on the EN pin when no system voltage above 2.5V is available, as shown in Figure 4. In this case, a  $100k\Omega$  pull-up resistor,  $R_{\text{EN}}$ , is connected between  $V_{\text{IN}}$  and the EN pin. MOSFET Q1 will be under logic control to pull down the EN pin.

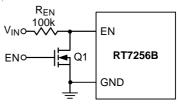


Figure 4. Digital Enable Control Circuit



#### **Under Voltage Protection**

#### **Hiccup Mode**

For the RT7256BH, it provides Hiccup Mode Under Voltage Protection (UVP). When the  $V_{FB}$  voltage drops below 0.4V, the UVP function will be triggered to shut down switching operation. If the UVP condition remains for a period, the RT7256BH will retry automatically. When the UVP condition is removed, the converter will resume operation. The UVP is disabled during soft-start period.

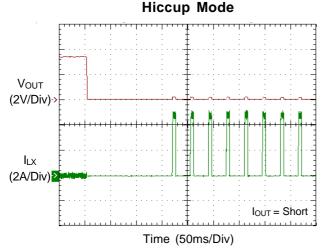


Figure 5. Hiccup Mode Under Voltage Protection

#### **Latch-Off Mode**

For the RT7256BL, it provides Latch-Off Mode Under Voltage Protection (UVP). When the FB voltage drops below half of the feedback reference voltage, V<sub>FB</sub>, UVP will be triggered and the RT7256BL will shut down in Latch-Off Mode. In shutdown condition, the RT7256BL can be reset by EN pin or power input VIN.

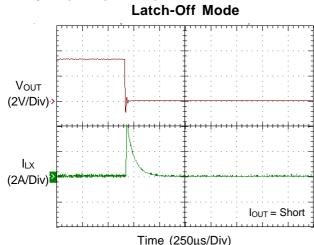


Figure 6. Latch-Off Mode Under Voltage Protection

#### **Over Temperature Protection**

The RT7256B features an Over Temperature Protection (OTP) circuitry to prevent from overheating due to excessive power dissipation. The OTP will shut down switching operation when junction temperature exceeds 150°C. Once the junction temperature cools down by approximately 20°C, the converter will resume operation. To maintain continuous operation, the maximum junction temperature should be lower than 125°C.

#### **Inductor Selection**

The inductor value and operating frequency determine the ripple current according to a specific input and output voltage. The ripple current  $\Delta I_L$  increases with higher  $V_{IN}$  and decreases with higher inductance.

$$\Delta I_{L} = \left[\frac{V_{OUT}}{f \times L}\right] \times \left[1 - \frac{V_{OUT}}{V_{IN}}\right]$$

Having a lower ripple current reduces not only the ESR losses in the output capacitors but also the output voltage ripple. High frequency with small ripple current can achieve the highest efficiency operation. However, it requires a large inductor to achieve this goal.

For the ripple current selection, the value of  $\Delta I_L = 0.24 (I_{MAX})$  will be a reasonable starting point. The largest ripple current occurs at the highest  $V_{IN}$ . To guarantee that the ripple current stays below the specified maximum, the inductor value should be chosen according to the following equation :

$$L = \left[ \frac{V_{OUT}}{f \times \Delta I_{L(MAX)}} \right] \times \left[ 1 - \frac{V_{OUT}}{V_{IN(MAX)}} \right]$$

The inductor's current rating (caused a 40°C temperature rising from 25°C ambient) should be greater than the maximum load current and its saturation current should be greater than the short circuit peak current limit. Please see Table 2 for the inductor selection reference.

Table 2. Suggested Inductors for	Typical
Application Circuit	

Component Supplier	Series	Dimensions (mm)		
TDK	VLF10045	10 x 9.7 x 4.5		
TDK	SLF12565	12.5 x 12.5 x 6.5		
TAIYO YUDEN	NR8040	8 x 8 x 4		
TAIYO YUDEN	NRS8040	8 x 8 x 4		

#### C<sub>IN</sub> and C<sub>OUT</sub> Selection

The input capacitance,  $C_{IN}$ , is needed to filter the trapezoidal current at the source of the high side MOSFET. To prevent large ripple current, a low ESR input capacitor sized for the maximum RMS current should be used. The approximate RMS current equation is given:

$$I_{RMS} = I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}}} - 1$$

This formula has a maximum at  $V_{IN} = 2V_{OUT}$ , where  $I_{RMS} = I_{OUT}$  / 2. This simple worst case condition is commonly used for design because even significant deviations do not offer much relief.

Choose a capacitor rated at a higher temperature than required. Several capacitors may also be paralleled to meet size or height requirements in the design.

For the input capacitor, two  $10\mu F$  low ESR ceramic capacitors are suggested. For the suggested capacitor, please refer to table 3 for more details.

The selection of  $C_{\text{OUT}}$  is determined by the required ESR to minimize voltage ripple.

Moreover, the amount of bulk capacitance is also a key for  $C_{\text{OUT}}$  selection to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response as described in a later section.

The output ripple,  $\Delta V_{OUT}$ , is determined by :

$$\Delta V_{OUT} \leq \Delta I_L \Bigg[ ESR + \frac{1}{8fC_{OUT}} \Bigg]$$

The output ripple will be the highest at the maximum input voltage since ΔI<sub>L</sub> increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirement. Dry tantalum, special polymer, aluminum electrolytic and ceramic capacitors are all available in surface mount packages. Special polymer capacitors offer very low ESR value. However, it provides lower capacitance density than other types. Although Tantalum capacitors have the highest capacitance density, it is important to only use types that pass the surge test for use in switching power supplies. Aluminum electrolytic capacitors have significantly higher ESR. However, it can be used in cost-sensitive applications for ripple current rating and long term reliability considerations. Ceramic capacitors have excellent low ESR characteristics but can have a high voltage coefficient and audible piezoelectric effects. The high Q of ceramic capacitors with trace inductance can also lead to significant ringing.

Higher values, lower cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal for switching regulator applications. However, care must be taken when these capacitors are used at input and output. When a ceramic capacitor is used at the input and the power is supplied by a wall adapter through long wires, a load step at the output can induce ringing at the input,  $V_{\text{IN}}$ . At best, this ringing can couple to the output and be mistaken as loop instability. At worst, a sudden inrush of current through the long wires can potentially cause a voltage spike at  $V_{\text{IN}}$  large enough to damage the part.

#### **Checking Transient Response**

The regulator loop response can be checked by looking at the load transient response. Switching regulators take several cycles to respond to a step in load current. When a load step occurs,  $V_{OUT}$  immediately shifts by an amount equal to  $\Delta I_{LOAD}$  (ESR) also begins to charge or discharge  $C_{OUT}$  generating a feedback error signal for the regulator to return  $V_{OUT}$  to its steady-state value. During this recovery time,  $V_{OUT}$  can be monitored for overshoot or ringing that would indicate a stability problem.

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#### **Thermal Considerations**

For continuous operation, do not exceed the maximum operation junction temperature 125°C. The maximum power dissipation depends on the thermal resistance of IC package, PCB layout, the rate of surroundings airflow and temperature difference between junction to ambient. The maximum power dissipation can be calculated by following formula:

$$P_{D(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$$

Where T<sub>J(MAX)</sub> is the maximum operation junction temperature ,  $T_{\text{A}}$  is the ambient temperature and the  $\theta_{\text{JA}}\text{is}$ the junction to ambient thermal resistance.

For recommended operating conditions specification of RT7256B, the maximum junction temperature is 125°C. The junction to ambient thermal resistance  $\theta_{JA}$  is layout dependent. For SOP-8 (Exposed Pad) package, the thermal resistance  $\theta_{JA}$  is 75°C/W on the standard JEDEC 51-7 four-layers thermal test board. The maximum power dissipation at  $T_A = 25^{\circ}C$  can be calculated by following formula:

 $P_{D(MAX)} = (125^{\circ}C - 25^{\circ}C) / (75^{\circ}C/W) = 1.333W$ (min.copper area PCB layout)

 $P_{D(MAX)} = (125^{\circ}C - 25^{\circ}C) / (49^{\circ}C/W) = 2.04W$ (70mm<sup>2</sup>copper area PCB layout)

The thermal resistance  $\theta_{JA}$  of SOP-8 (Exposed Pad) is determined by the package architecture design and the PCB layout design. However, the package architecture design had been designed. If possible, it's useful to increase thermal performance by the PCB layout copper design. The thermal resistance  $\theta_{JA}$  can be decreased by adding copper area under the exposed pad of SOP-8 (Exposed Pad) package.

As shown in Figure 7, the amount of copper area to which the SOP-8 (Exposed Pad) is mounted affects thermal performance. When mounted to the standard SOP-8 (Exposed Pad) pad (Figure 7.a), θ<sub>JA</sub> is 75°C/W. Adding copper area of pad under the SOP-8 (Exposed Pad) (Figure 7.b) reduces the  $\theta_{JA}$  to 64°C/W. Even further, increasing the copper area of pad to 70mm<sup>2</sup> (Figure 7.e) reduces the  $\theta_{JA}$  to 49°C/W.

The maximum power dissipation depends on operating

ambient temperature for fixed  $T_{J(MAX)}$  and thermal resistance  $\theta_{JA}$ . For RT7256B packages, the Figure 8 of derating curves allows the designer to see the effect of rising ambient temperature on the maximum power dissipation allowed.

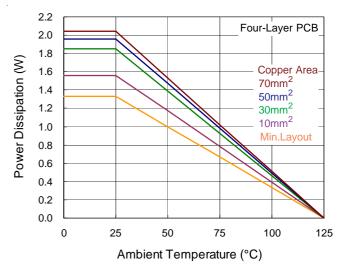
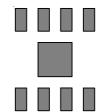
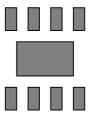


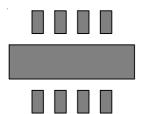
Figure 8. Derating Curves for RT7256B Package



(a) Copper Area =  $(2.3 \times 2.3) \text{ mm}^2$ ,  $\theta_{JA} = 75^{\circ}\text{C/W}$ 



(b) Copper Area =  $10 \text{mm}^2$ ,  $\theta_{JA} = 64 ^{\circ} \text{C/W}$ 



(c) Copper Area =  $30 \text{mm}^2$ ,  $\theta_{JA} = 54^{\circ}\text{C/W}$ 



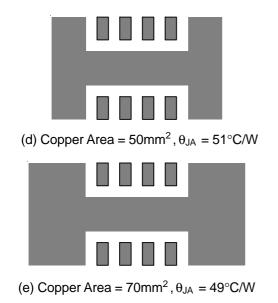
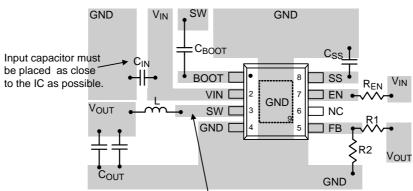


Figure 7. Thermal Resistance vs. Copper Area Layout Design

#### **Layout Consideration**

Follow the PCB layout guidelines for optimal performance of the RT7256B.

- Keep the traces of the main current paths as short and wide as possible.
- Put the input capacitor as close as possible to the device pins (VIN and GND).
- SW node is with high frequency voltage swing and should be kept at small area. Keep analog components away from the SW node to prevent stray capacitive noise pick-up.
- An example of PCB layout guide is shown in Figure 9 for reference.



SW node is with high frequency voltage swing and should be kept at small area. Keep analog components away from the SW node to prevent stray capacitive noise pick-up

Figure 9. PCB Layout Guide

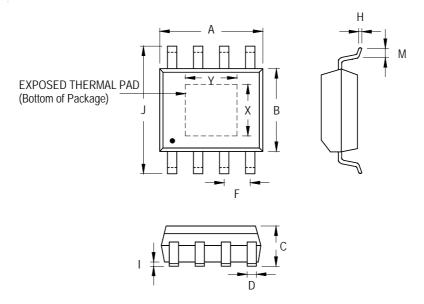
Table 3. Suggested Capacitors for CIN and COUT

Location	Component Supplier	Part No.	Capacitance (μF)	Case Size
C <sub>IN</sub>	MURATA	GRM31CR61E106K	10	1206
C <sub>IN</sub>	TDK	C3225X5R1E106K	10	1206
C <sub>IN</sub>	TAIYO YUDEN	TMK316BJ106ML	10	1206
C <sub>OUT</sub>	MURATA	GRM31CR60J476M	47	1206
Соит	TDK	C3225X5R0J476M	47	1210
C <sub>OUT</sub>	MURATA	GRM32ER71C226M	22	1210
C <sub>OUT</sub>	TDK	C3225X5R1C22M	22	1210

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## **Outline Dimension**



Symbol		Dimensions I	n Millimeters	Dimensions In Inches		
		Min	Max	Min	Max	
Α		4.801	5.004	0.189	0.197	
В		3.810	4.000	0.150	0.157	
С		1.346	1.753	0.053	0.069	
D		0.330	0.510	0.013	0.020	
F	F		1.346	0.047	0.053	
Н		0.170	0.254	0.007	0.010	
1		0.000	0.152	0.000	0.006	
J		5.791	6.200	0.228	0.244	
М		0.406	1.270	0.016	0.050	
Ontinu 4	Х	2.000	2.300	0.079	0.091	
Option 1	Υ	2.000	2.300	0.079	0.091	
Ontion 2	Х	2.100	2.500	0.083	0.098	
Option 2	Υ	3.000	3.500	0.118	0.138	

8-Lead SOP (Exposed Pad) Plastic Package

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